



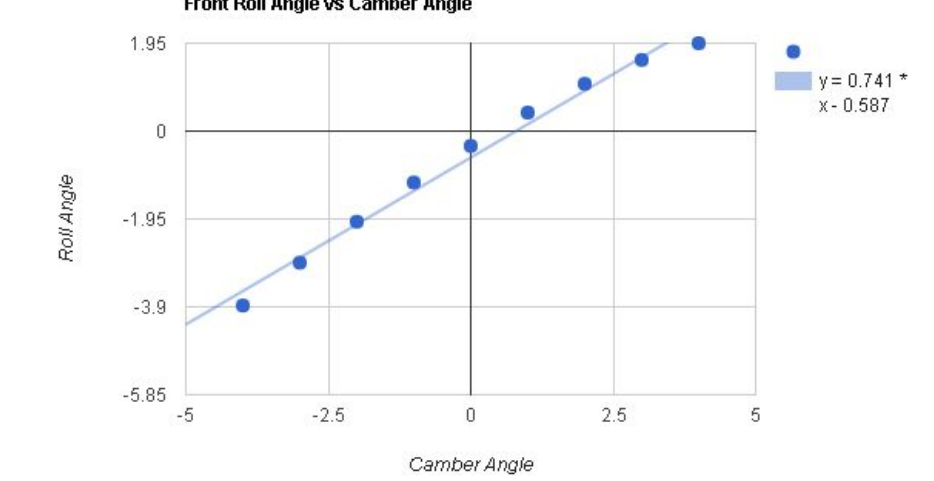
FSAE Racecar: AR-12 "Mantis"

Advisers: Dr. Michael McCarthy, Robert "Smitty" Smith, Phil Chipman

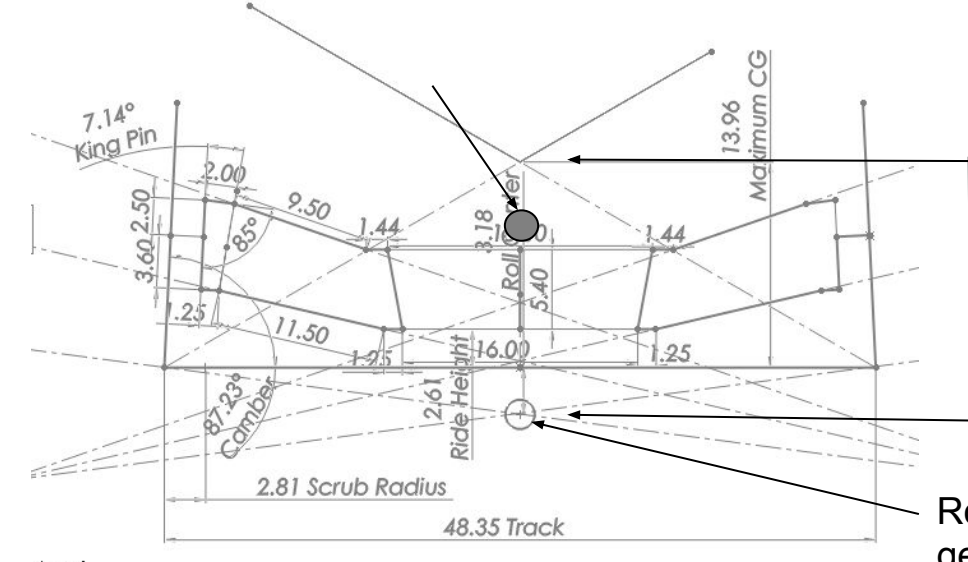


Suspension: Suspension design for AR-12 Mantis began with identifying the problems with last year's car, AR-11 Savage. A high vertical center of gravity was the vehicle's biggest enemy, which resulted in disqualification from competition after the car nearly rolled over under high cornering loads. Many of the 2014-2015 catastrophic design faults had been addressed with Savage last year, which provided a great starting point for this year's design. Design goals for Mantis include; lowering the vertical c.g., reducing the force required to turn steering wheel, Incorporation of anti-roll bars (reducing body roll and adjustable handling characteristics), optimizing suspension geometry to utilize as much contact patch as possible.

Old Camber Angle VS. Body Roll



Savage's Scrub Radius- 2.8 inches, and car was heavy. Mantis' Scrub radius - 1.25 in. Wheel effort force is a function of scrub radius

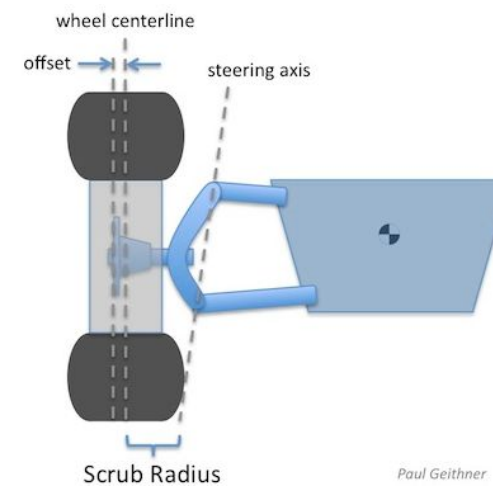
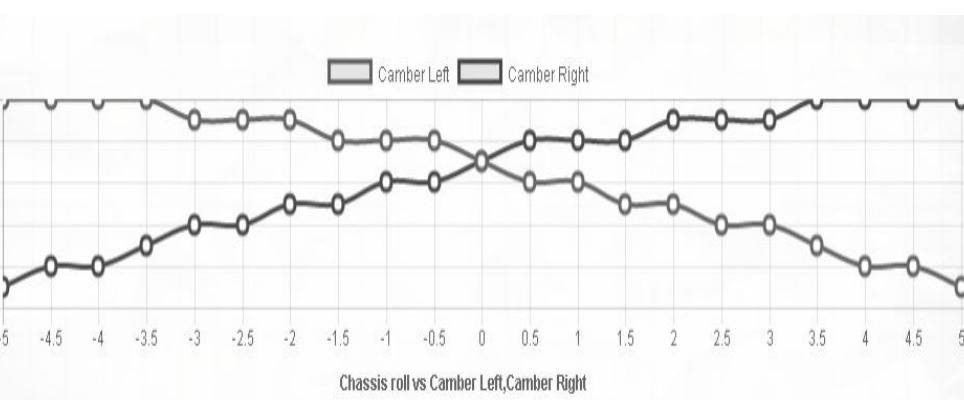


Roll Moment- This is the lever arm between C.G. and roll center

Roll Center - geometric point that the car rolls about

Savage had a vertical c.g. of 16 inches. Mantis' vertical C.G. is calculated to be 12.5 inches.

New Camber Angle VS. Body Roll



Chassis:

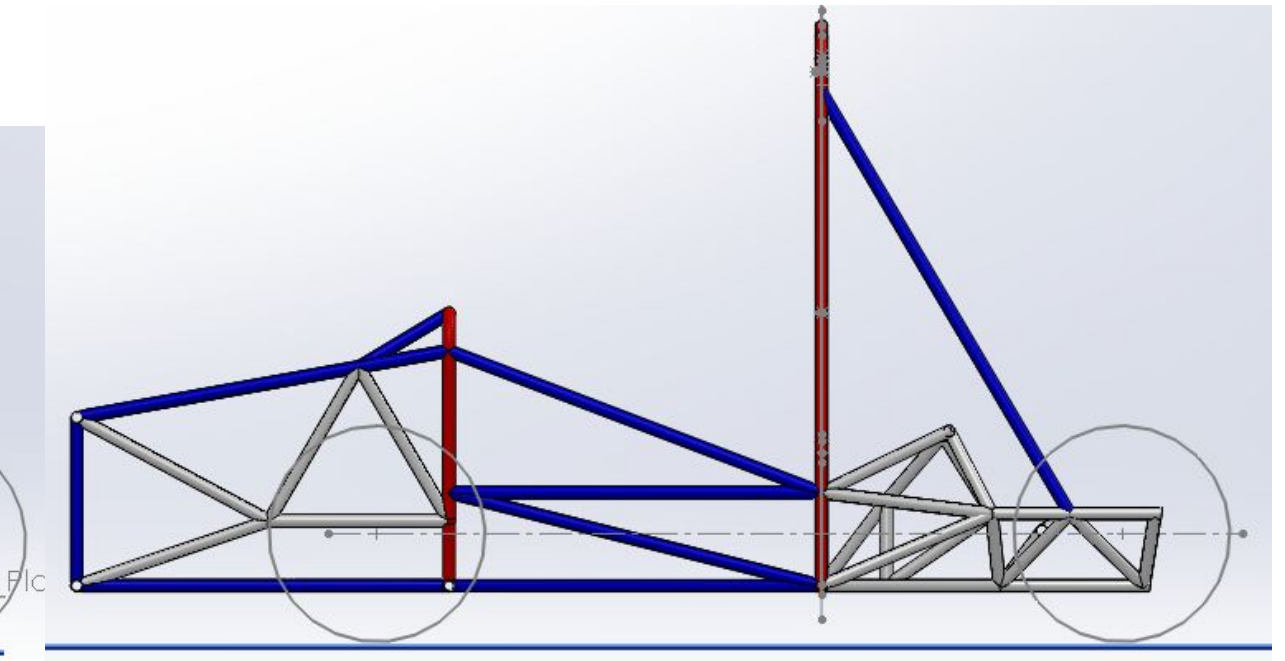
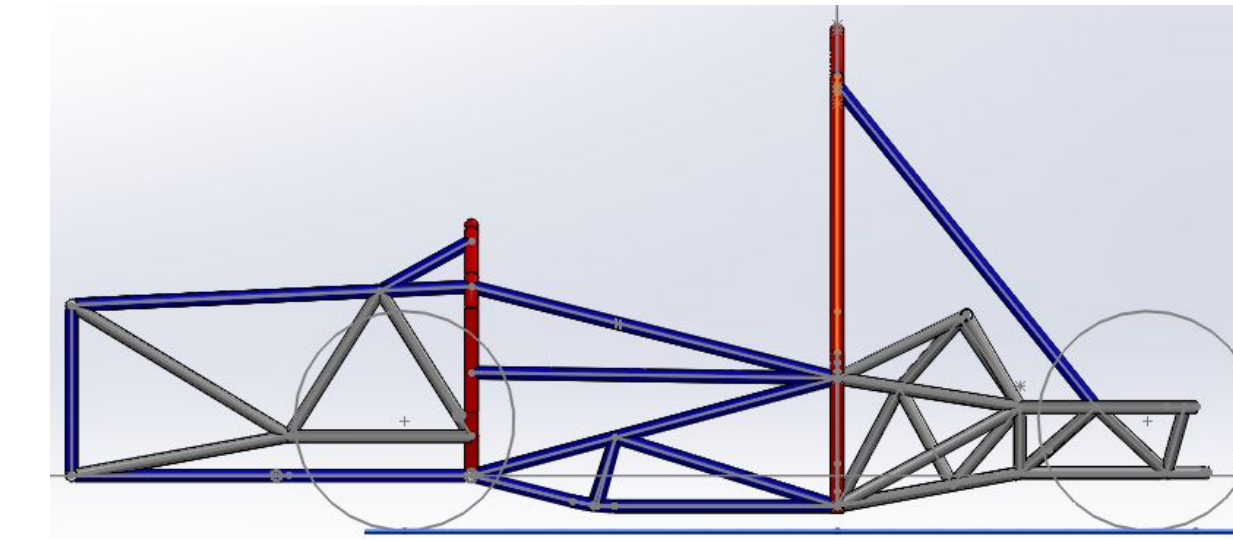
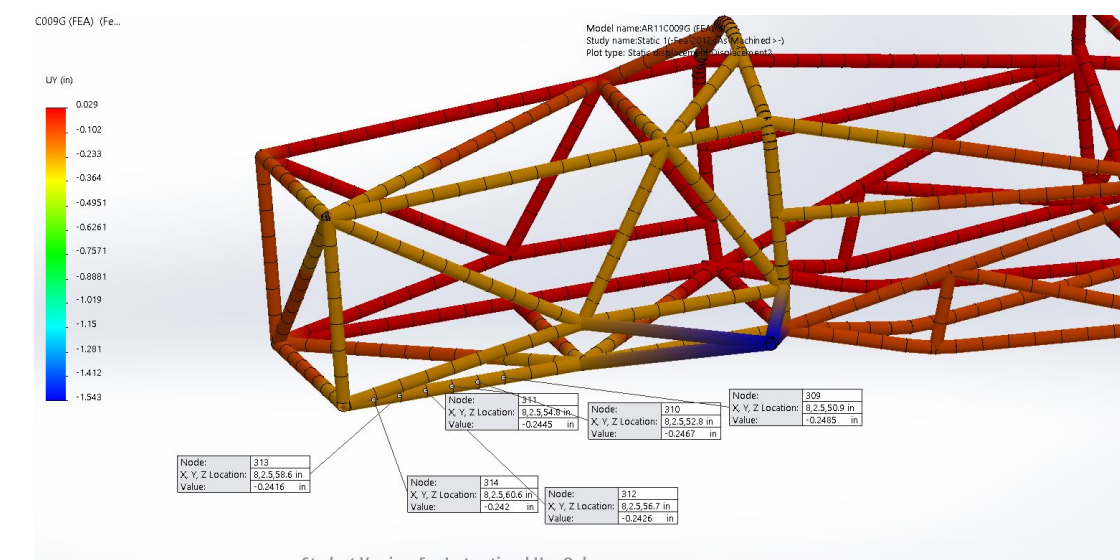
- Rules Compliant
 - Comply to the rules set by FSAE
- Lower Center of gravity
 - Lower center of car but keep nose and rear at original height for optimized suspension.
- Improved driver ergonomics
 - Reclined seat
 - Triangular shaped front roll hoop to give greater visibility
 - longer nose to accommodate reclined driver position
- Reduce weight
 - Smaller main roll hoop
- Strength
 - Torsional Rigidity minimum of 2000 lb/deg

This Year's Chassis:

- Theoretical weight
 - 76 lbs (no welds)
- Torsional Rigidity
 - $\Delta y = -0.2443$
 - $\Theta = 0.875^\circ$
 - 2286 lb/deg

Last Year's Chassis:

- Theoretical weight
 - 75 lbs (no welds)
- Torsional Rigidity
 - $\Delta y = -0.282$
 - $\Theta = 1.009^\circ$
 - 1982 lb/deg

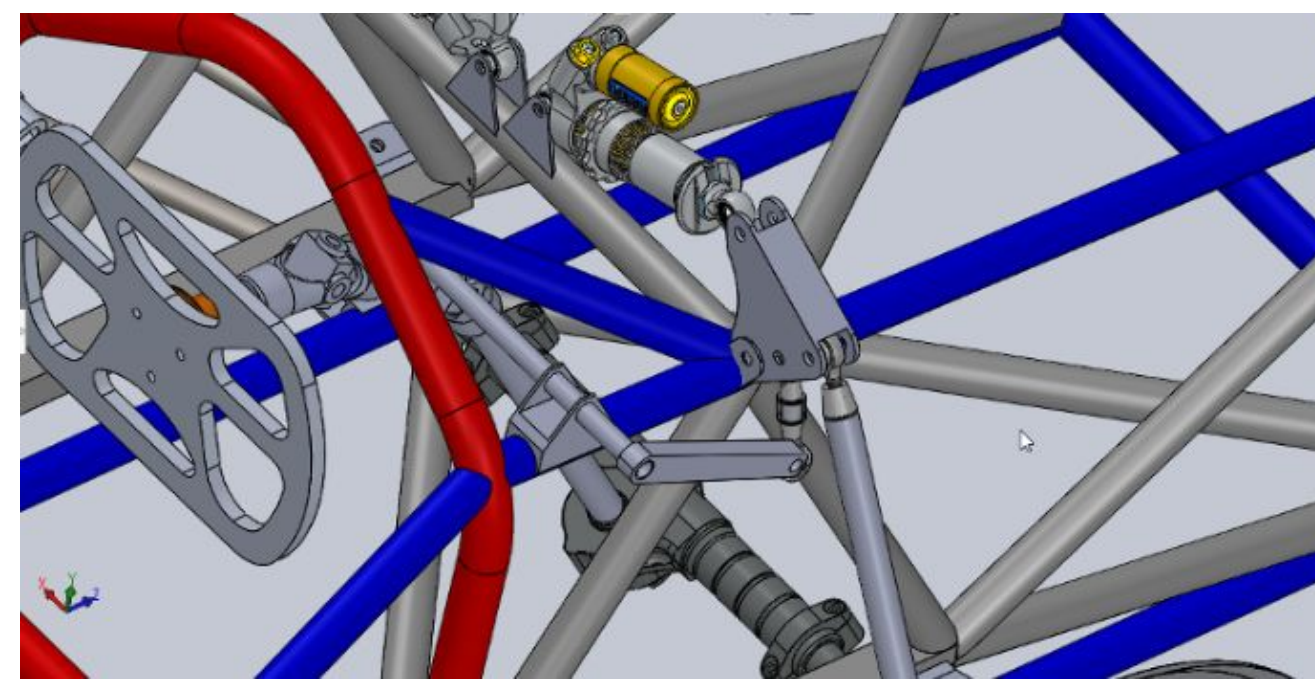


Human Interface:

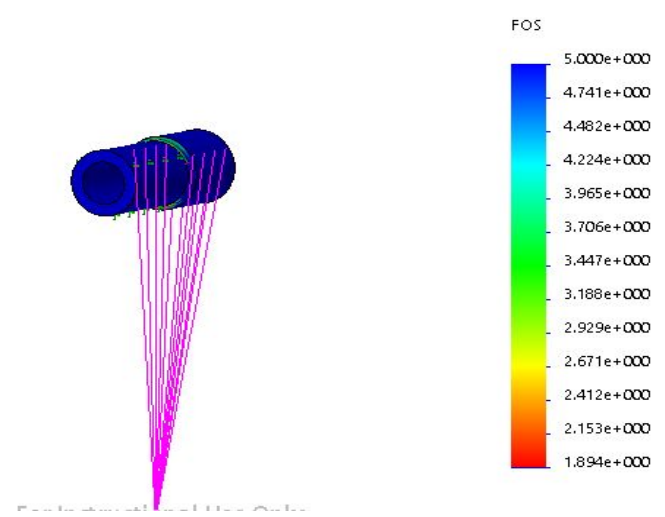
- Our main objective for the design of Human Interface components was to push the seat further back and to have a larger angle with reference taken from the vertical
 - The back support of the seat is angled at 42 degrees
 - Better visibility that is still FSAE rules compliant by having a span of 200 degrees (100 left and right)
- Using a 3/16" steering wheel thickness, it was tailored to have tailored 3" of clearance from the front roll-hoop
 - Steering wheel increased diameter size to 10.5", with flat cut outs on top and bottom to decrease steering effort

Optimization of Dynamic Camber- Wheel camber of 0 degrees at all times is desirable

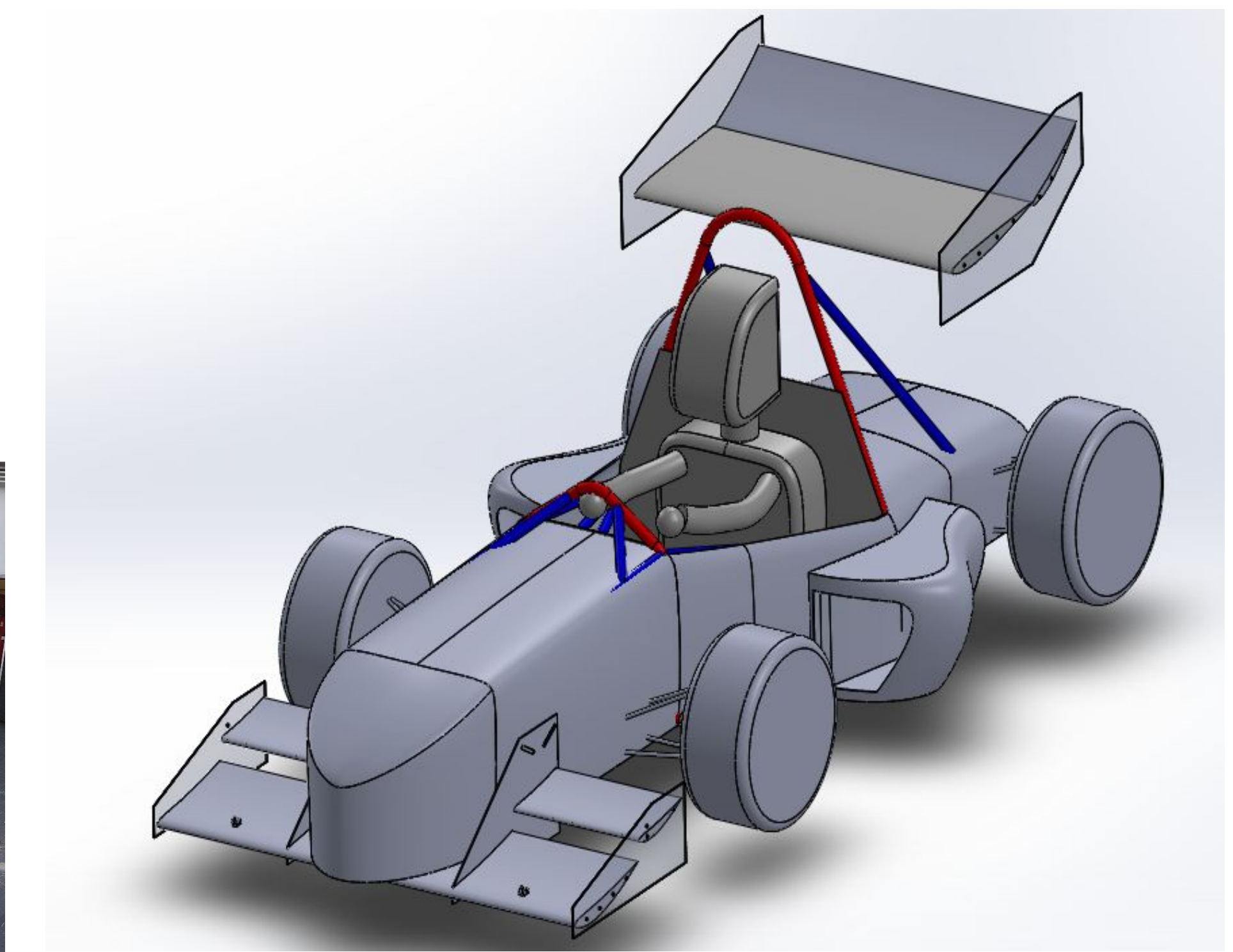
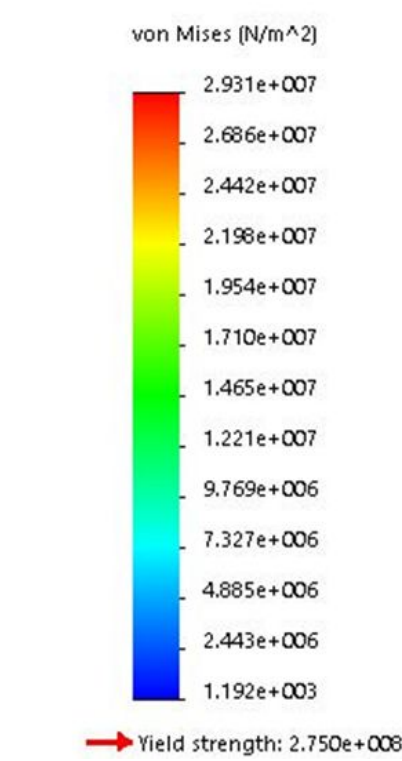
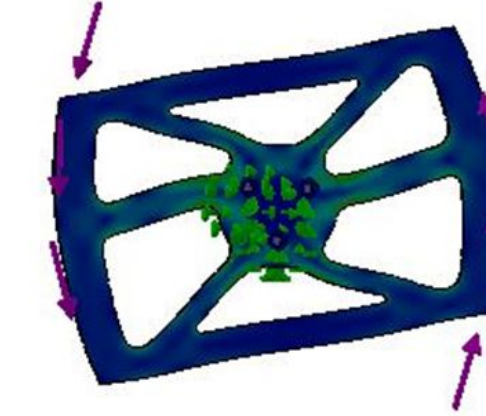
AR-12 Front Dampers and Sway Bar



Finite Element Analysis is performed to validate part's strength, here on our front spindle



Model name:Steering Wheel Template Study name:Static 1(-Default) Plot type:Static modal stress Stress1 Deformation scale: 324.792



Powertrain

Main Goal

Increase power to weight ratio, without sacrificing reliability

Objectives

- Optimize the packaging of all components
- Stronger and lighter parts

Packaging

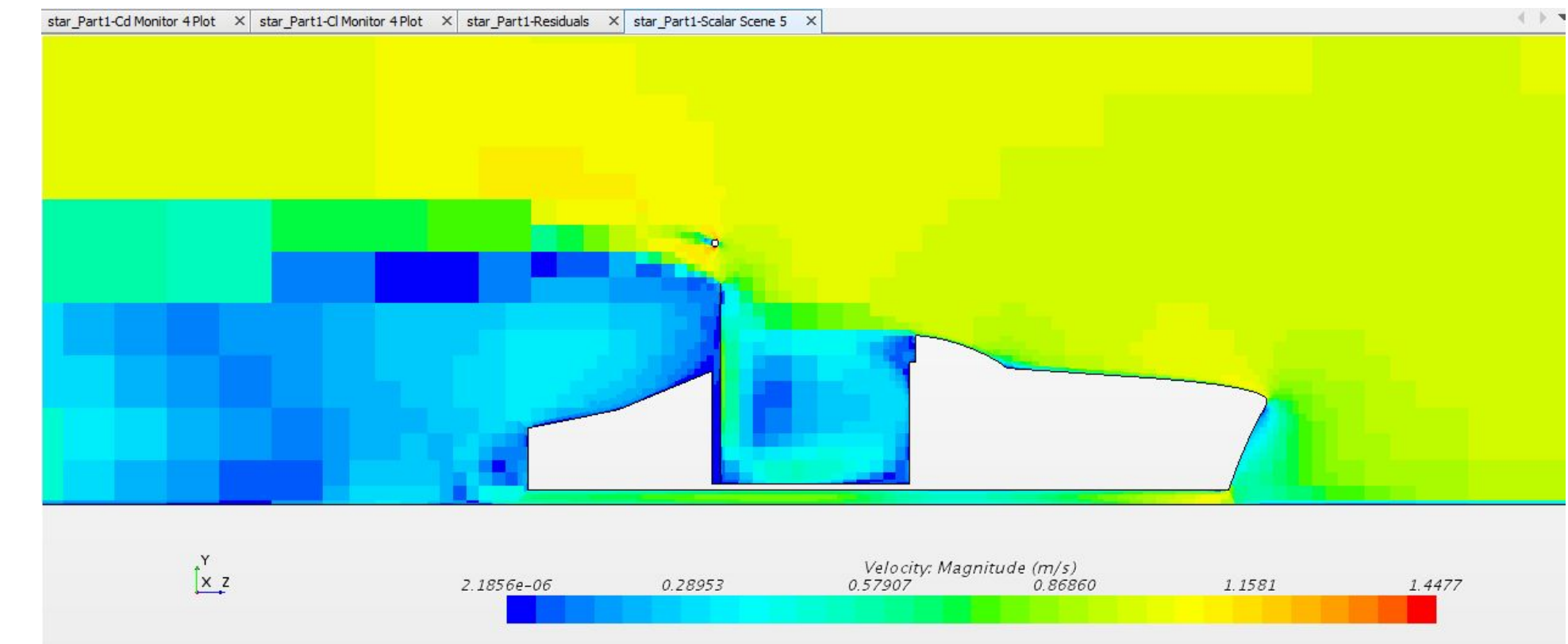
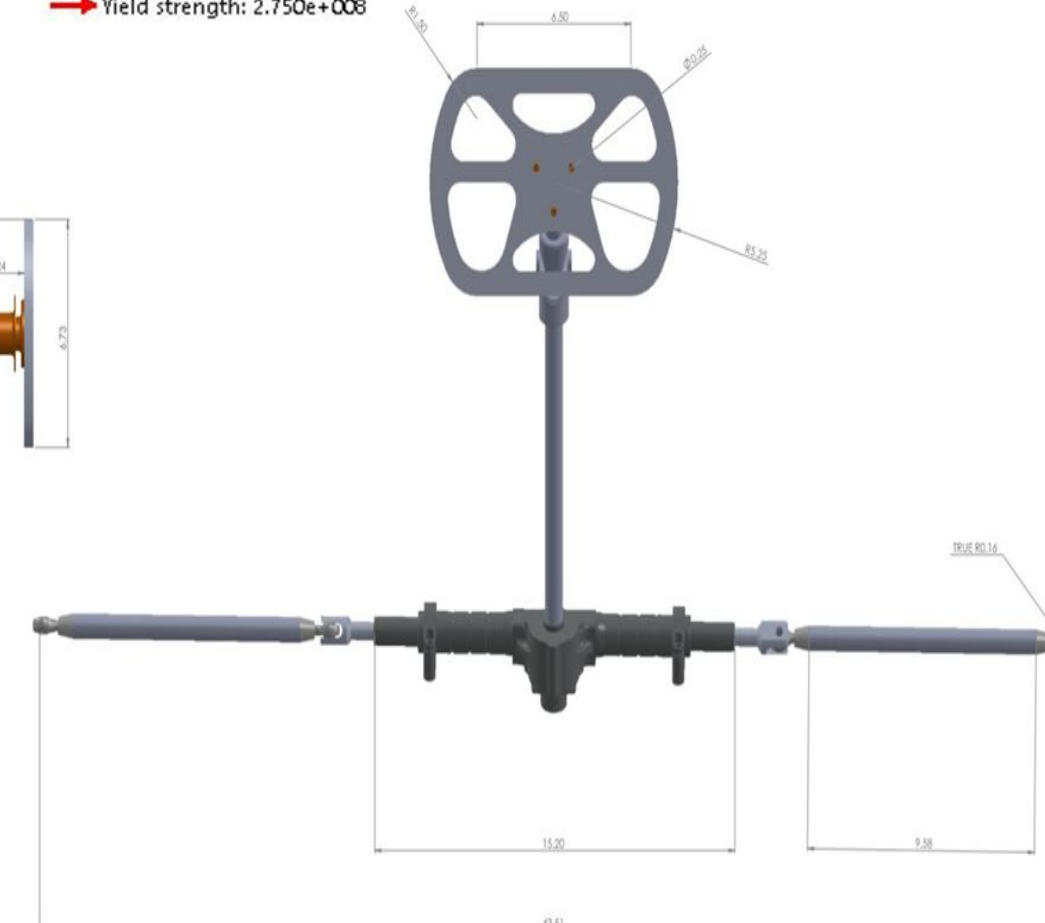
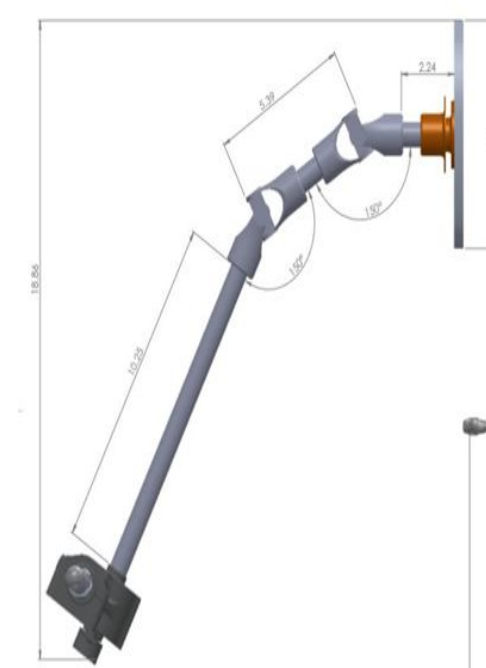
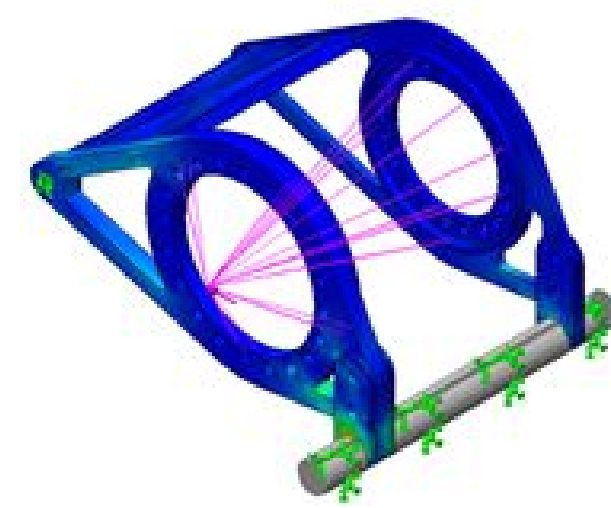
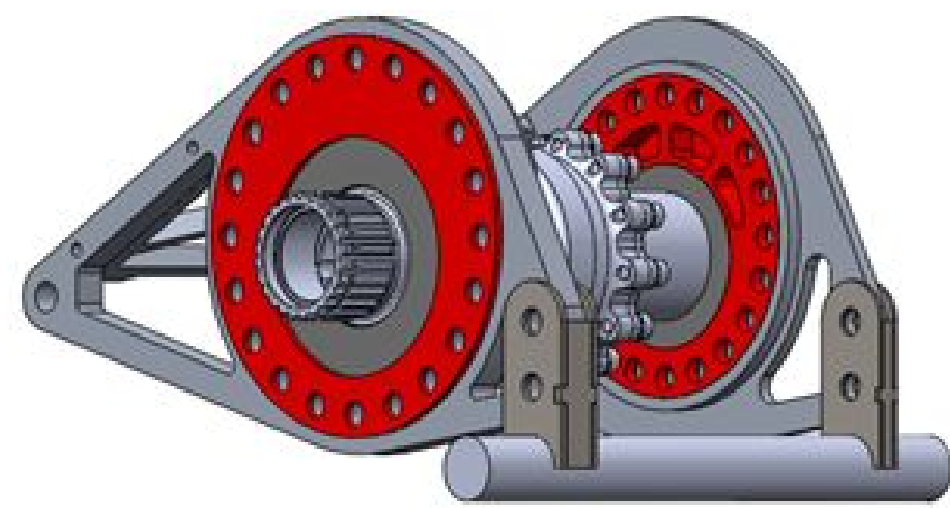
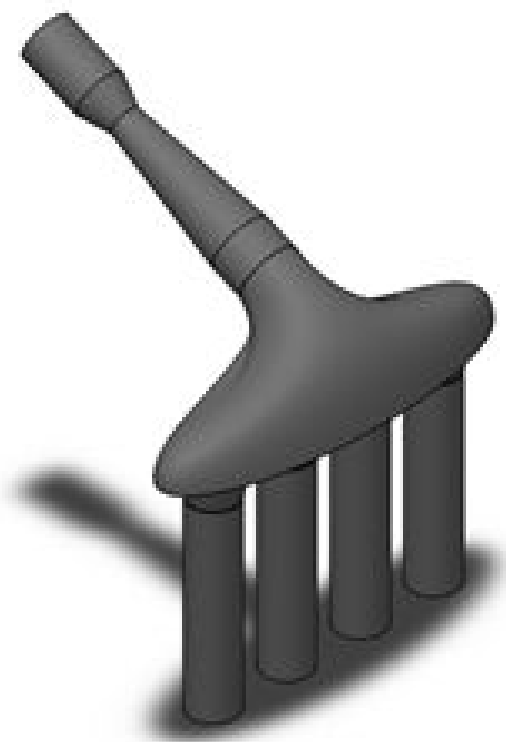
- Achieved lower center of gravity through lower engine placement

Drivetrain

- Features a ~ 3 lb lighter differential made by Drexler Motorsports
- Differential Carrier shown to withstand an expected 3200 lb chain force with FOS = 1.84

Air Induction System

- Intake manifold weight reduction of ~ 4 lbs, utilizing pre-preg carbon fiber
- Induced lower power band through enhanced runner dimensions



Chief Engineer: Matt Clark

Subteam Leads: Tomas Perez, Tim Zaragoza, Daniel Torres, George Bishara, Giovanni F. de Castro